

Urslau case study:
**A comparison of transport equations with
long-term monitored bedload data**

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Content

Study site - Urslau

Bedload monitoring methods

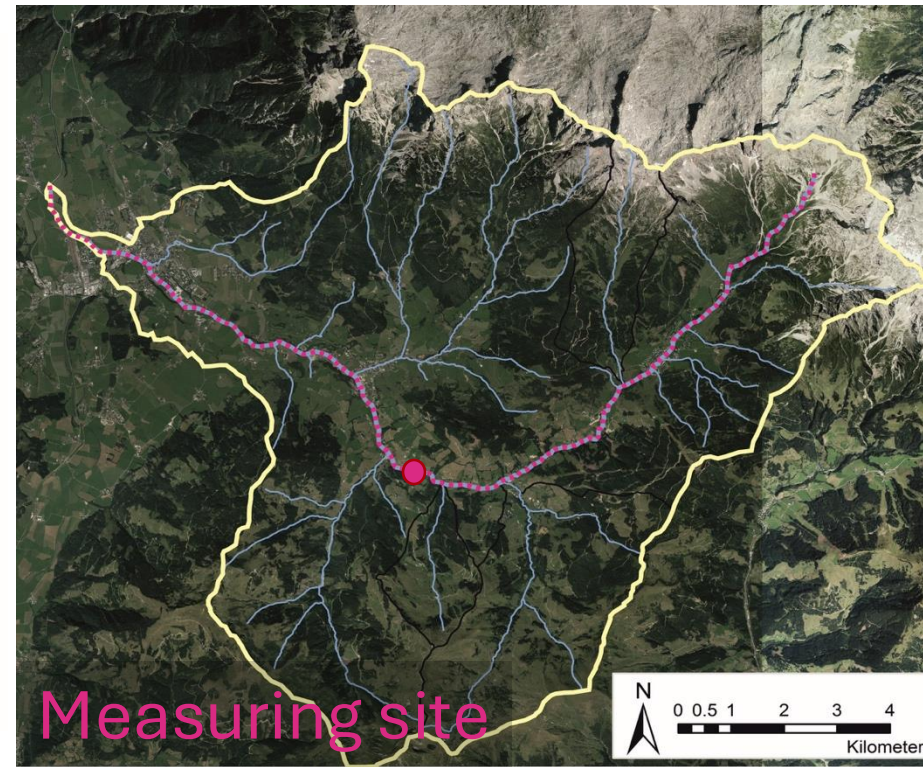
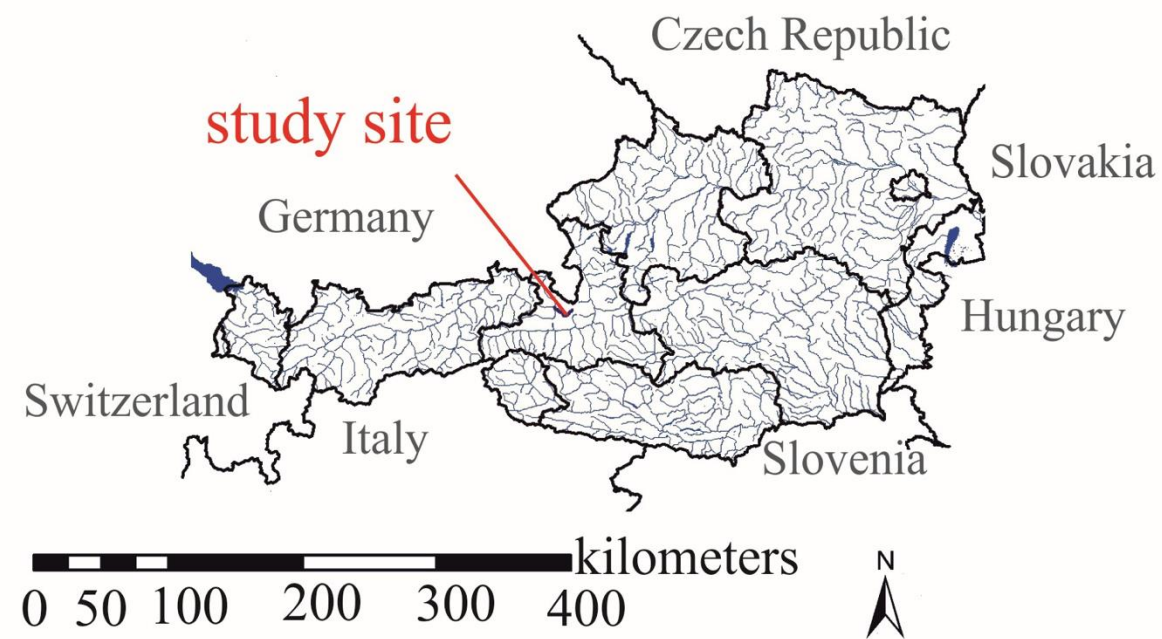
Bedload transport data

Measured vs. calculated bedload data

Conclusions



Study Site Urslau



- Europe / Austria / Salzburg
- Urslau stream
- Total flow length of 21.3 km
- Total catchment size: 122 km²
- Northern Limestone Alps, Greywacke

Steep upper reach



Middle reach



Bedload monitoring site



- Bedload monitoring site (since 2011)
- Catchment size: 56 km²
- Bed slope: 0.021
- Stream width: 8 m
- Bed material:
 $d_m = 0.05 \text{ m}$, $d_{90} = 0.09 \text{ m}$

Integrative Bedload Monitoring

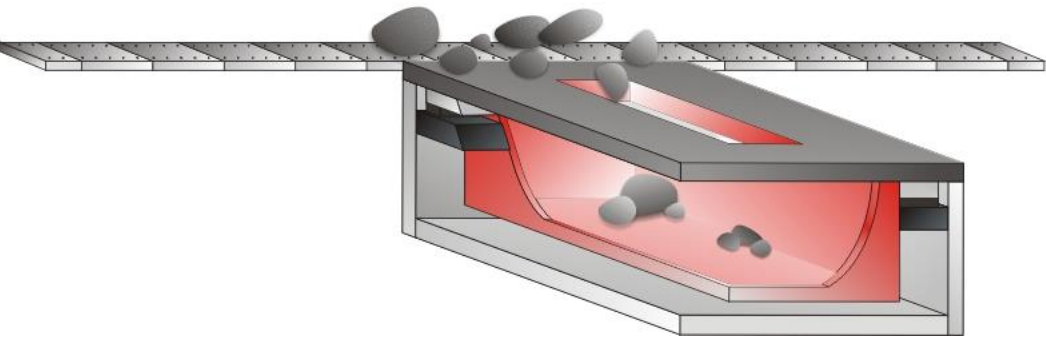
Mobile net sampler



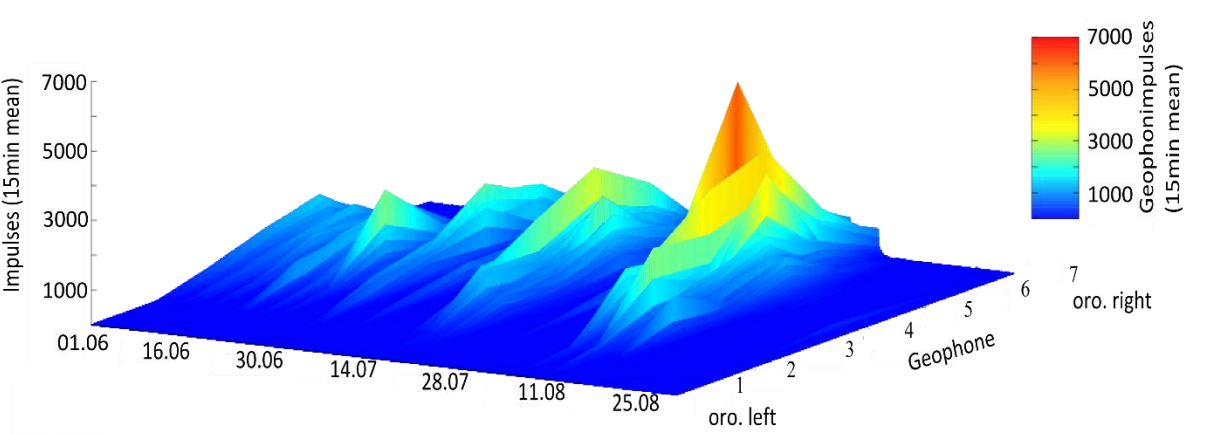
Plate Geophones



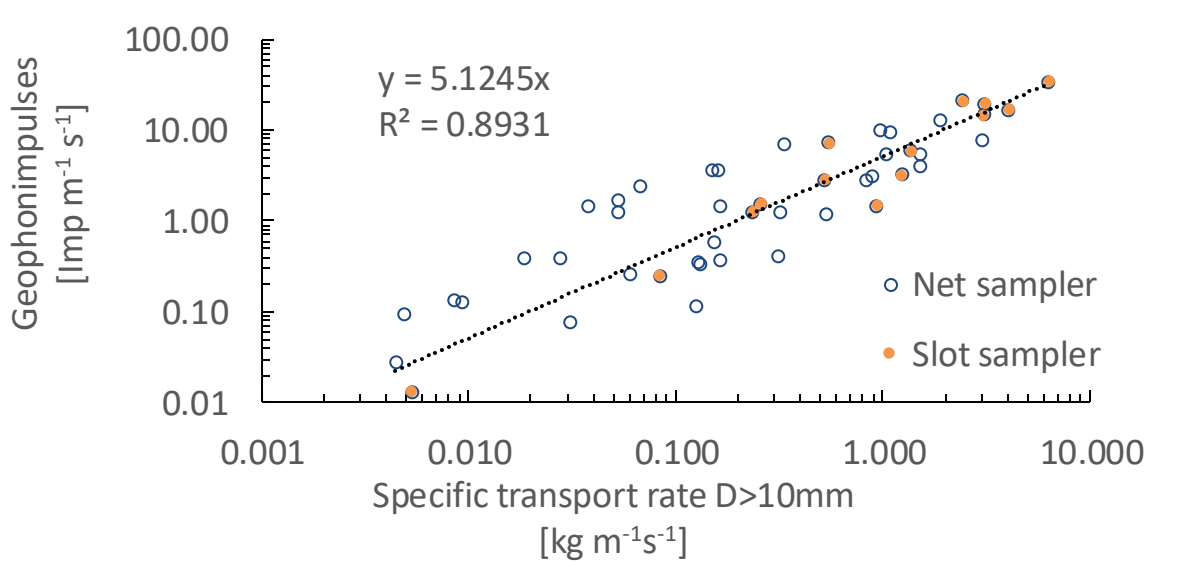
Slot sampler



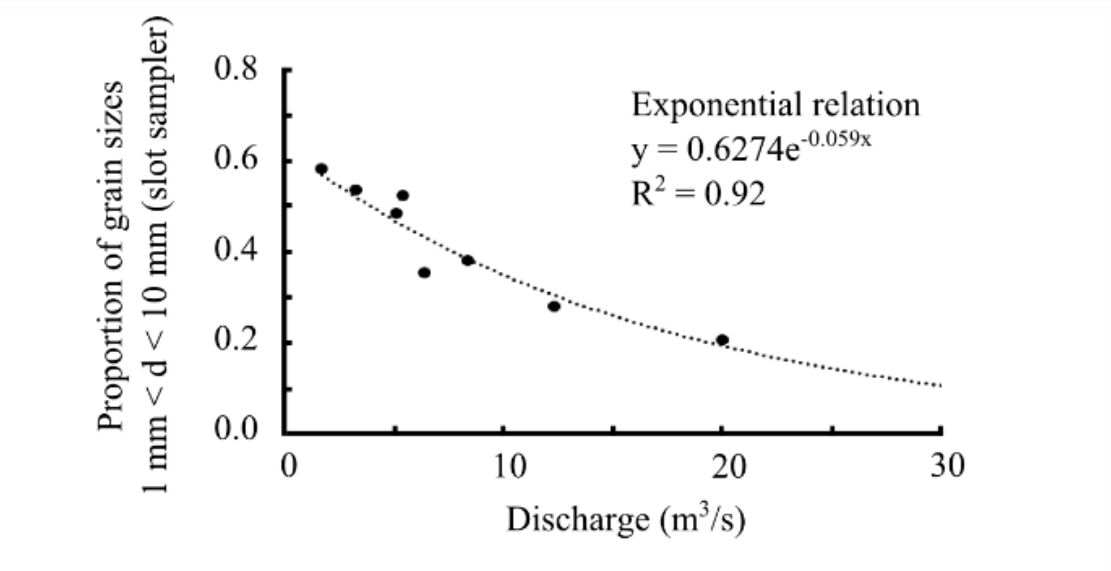
Continuous recording of Geophonimpulses (01.06.16-31.08.2016)

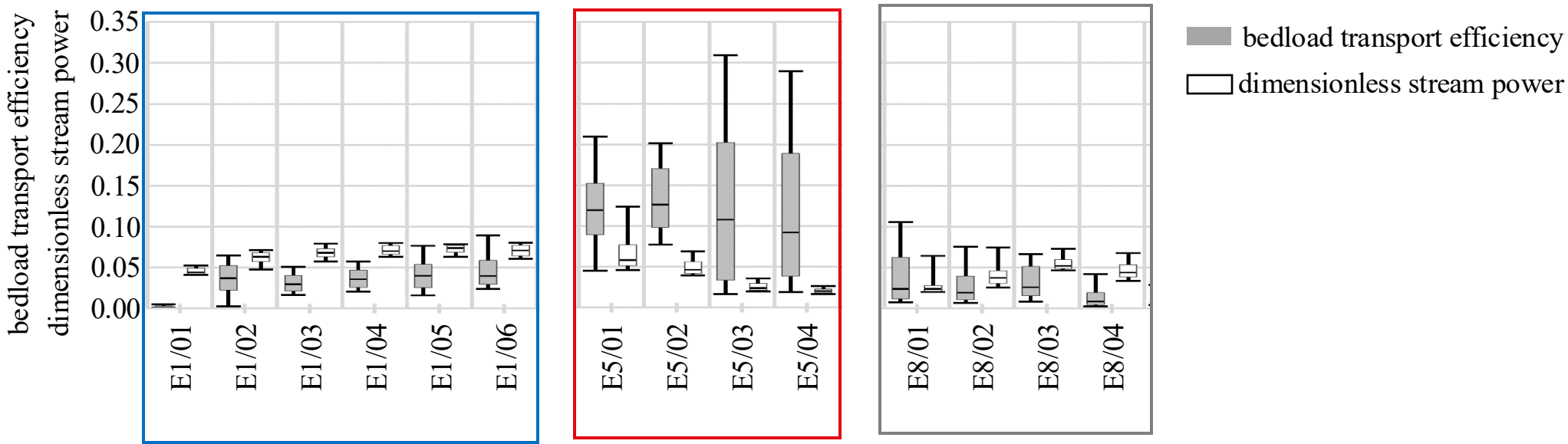
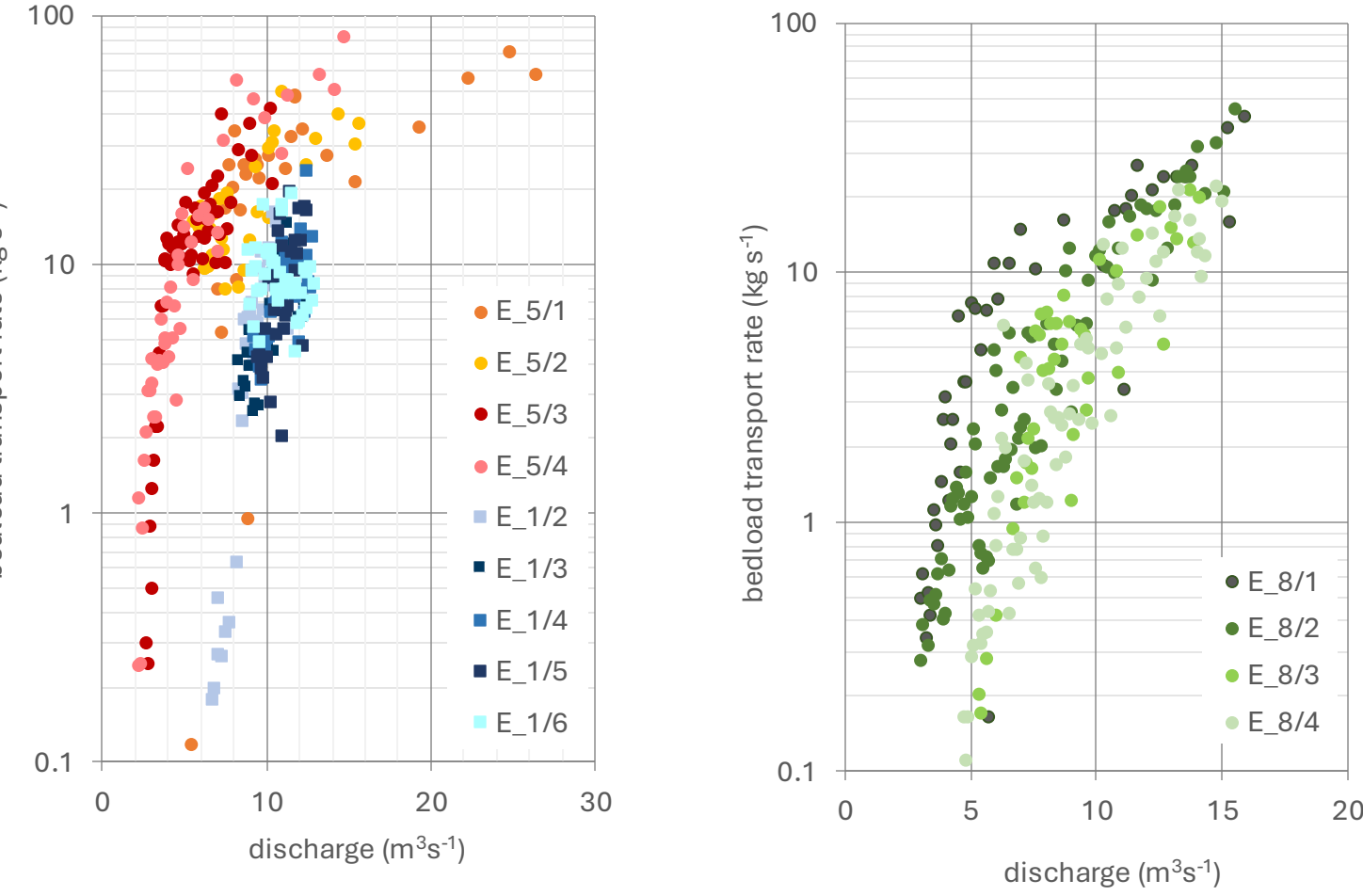
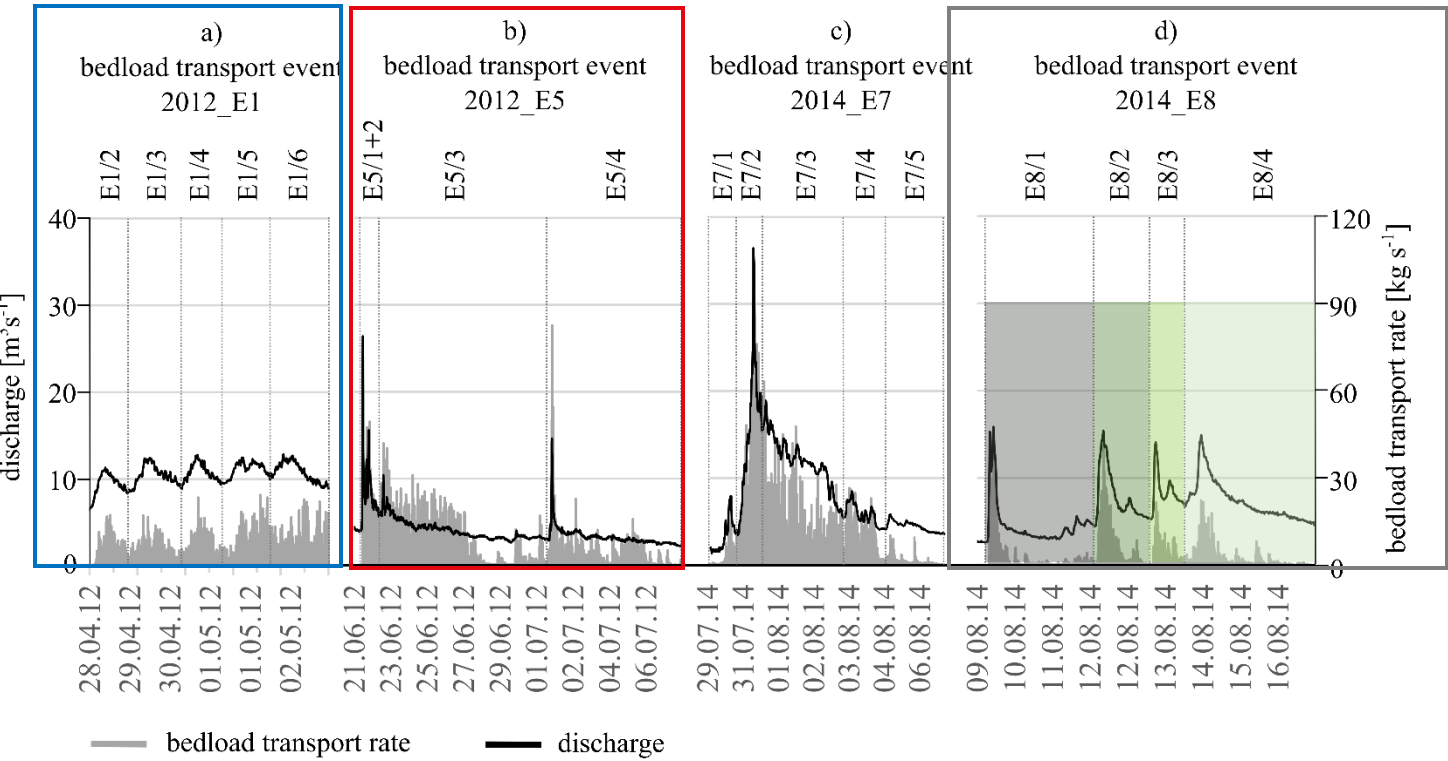


Calibration function



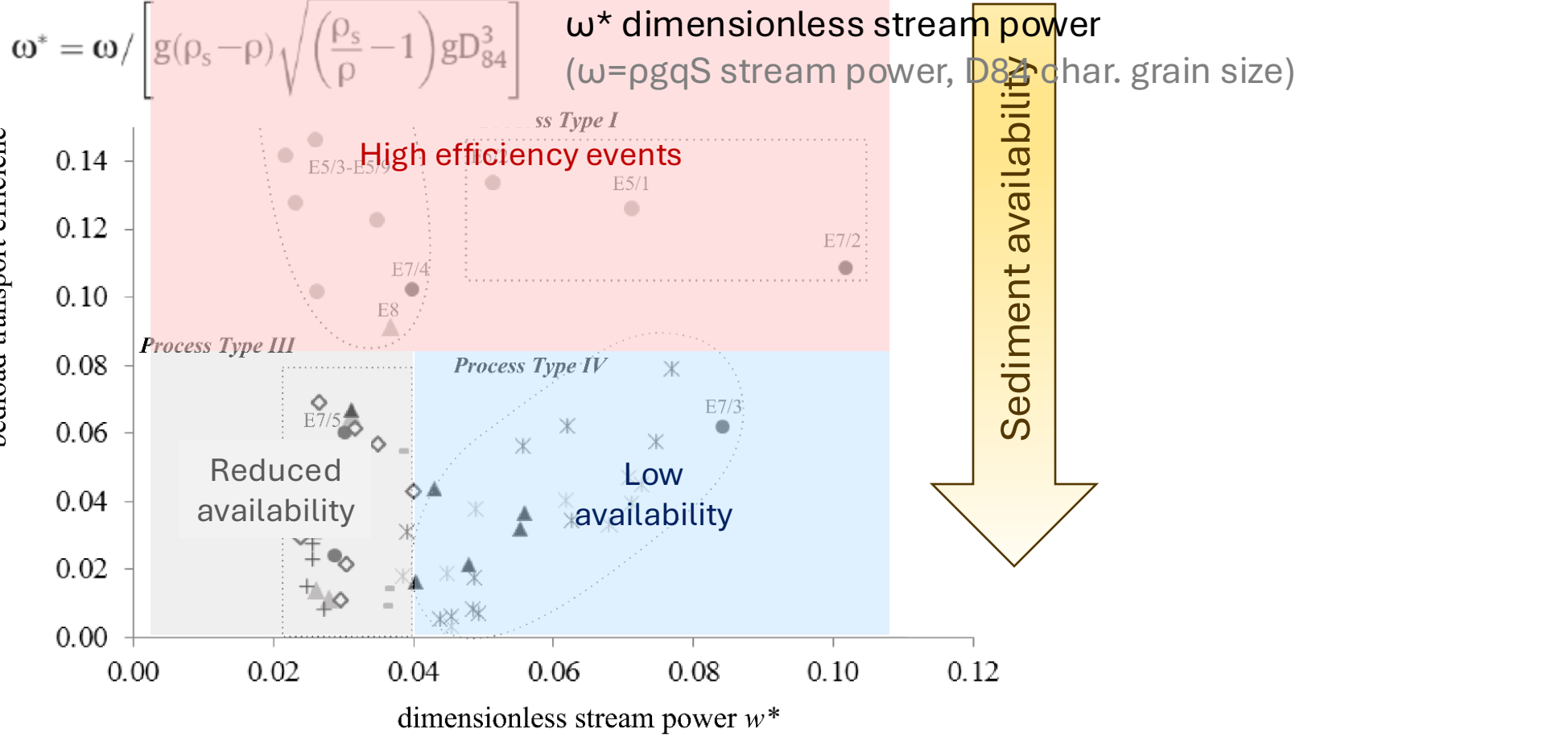
Proportion 1-10mm vs. discharge





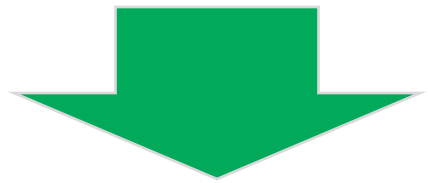
$$e_p = \frac{I_b \tan \alpha}{\Omega_{ex}}$$

e_p bedload transport efficiency (Bagnold, 1966)
(I_b immersed bedload volume, Ω_{ex} excess stream power, α inner fric. angle = 52°)



Long-term, integrative measured bedload data, high spatial variability

Process understanding, bedload transport event types



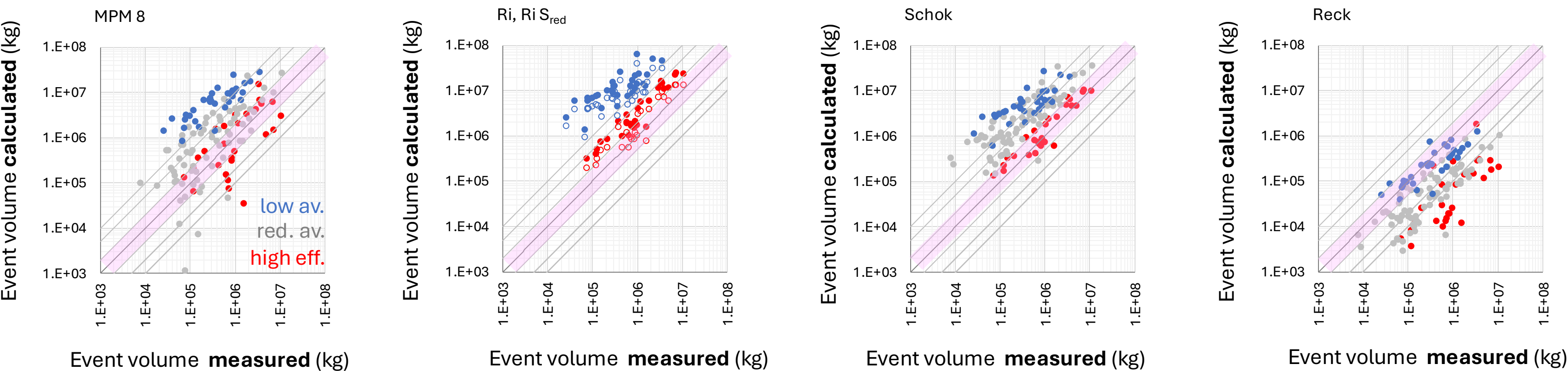
Evaluation of bedload transport formulas

- Development of bedload transport formulas (mostly) in laboratory settings
- Natural processes and transport dynamics not adequately considered
- Comparisons in the literature are typically based on point measurements

➤ **Continuous long-term data as a basis for evaluating calculation approaches**

1) Bedload volumes (kg) (data from 2011-2020)

Discrepancy factor $r_d = \frac{\text{calculated bedload}}{\text{measured bedload}}$



MPM-8 (Meyer-Peter and Mueller 1948)

$$\Phi_b = 8 * (\theta' - \theta_c)^{3/2}$$

θ' ...reduced dimensional boundary shear stress
 θ_c ...critical Shields number

Ri (Rickenmann 1990, 2001)

$$q_b = 1.5 * S^{1.5}(q - q_c)$$

q ...unit discharge
 q_c ...critical discharge at initiation of motion

Schok (Schoklitsch 1962)

$$q_b = \frac{2.5}{S} S^{1.5}(q - q_c)$$

q ...unit discharge
 q_c ...critical discharge at initiation of motion

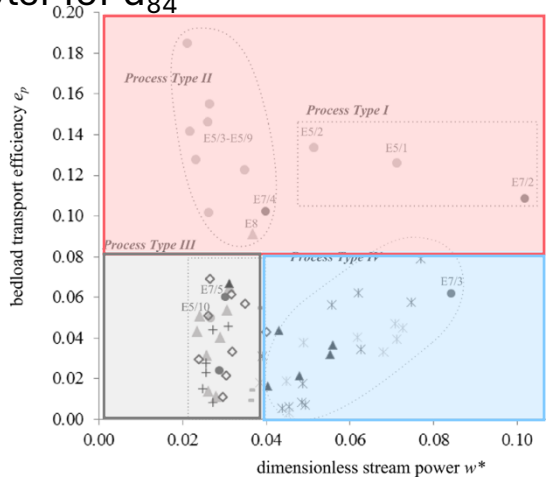
Reck (Recking 2013, 2016)

$$\Phi_{b,d84} = 14 \tau_{84}^{*2.5} / \left[1 + \left(\frac{\tau_m^*}{\tau_{84}^*} \right)^4 \right]$$

$\tau_m^* = 1.5 * S^{0.75}$ is the mobility shear stress
 τ_{84}^* = Shields parameter for d_{84}

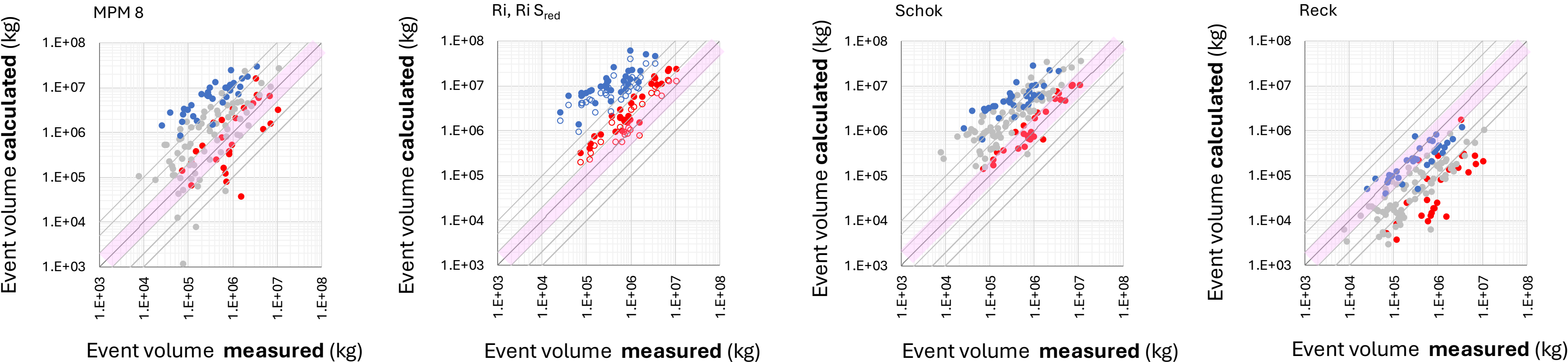
Ri_Sred (Rickenmann and Recking, 2011)

$$S_{red} = S \left(\sqrt{\frac{f_0}{f_{tot}}} \right)^e q_b \quad f_0/f_{tot} \text{ ...base roughness/total roughness}$$



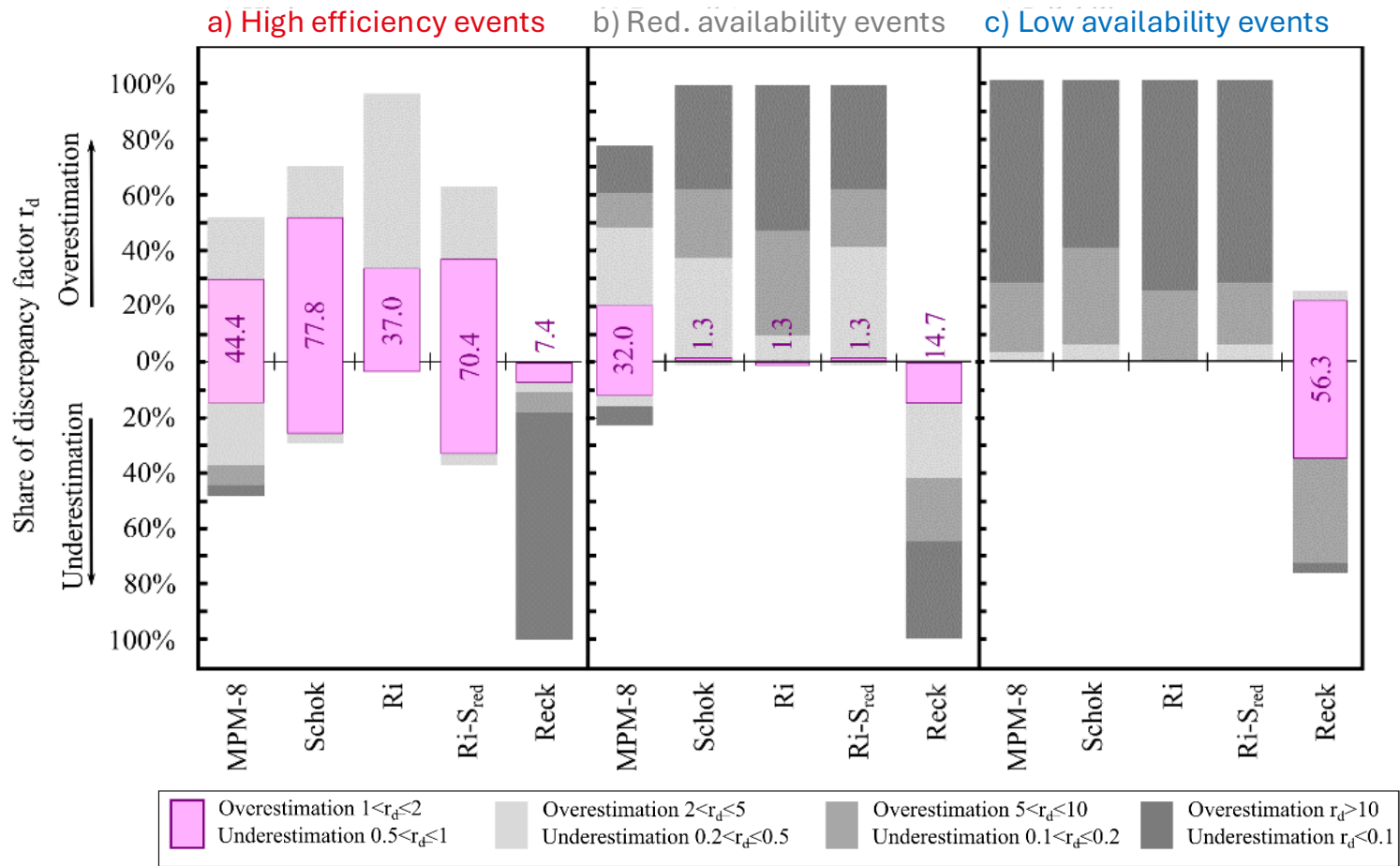
Measured vs. calculated bedload data – Event Volumes

(Lammer et al., *Sediment Research*, 2024)

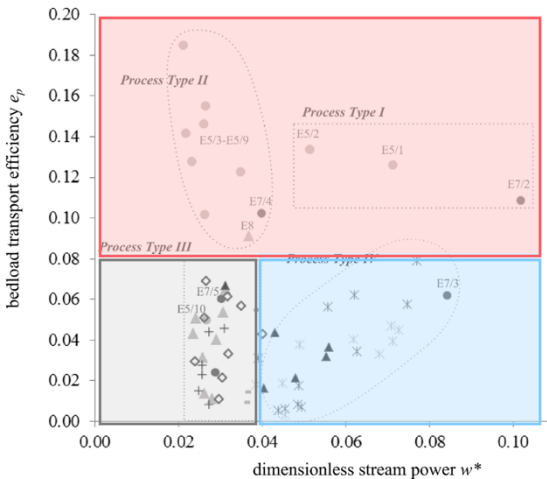


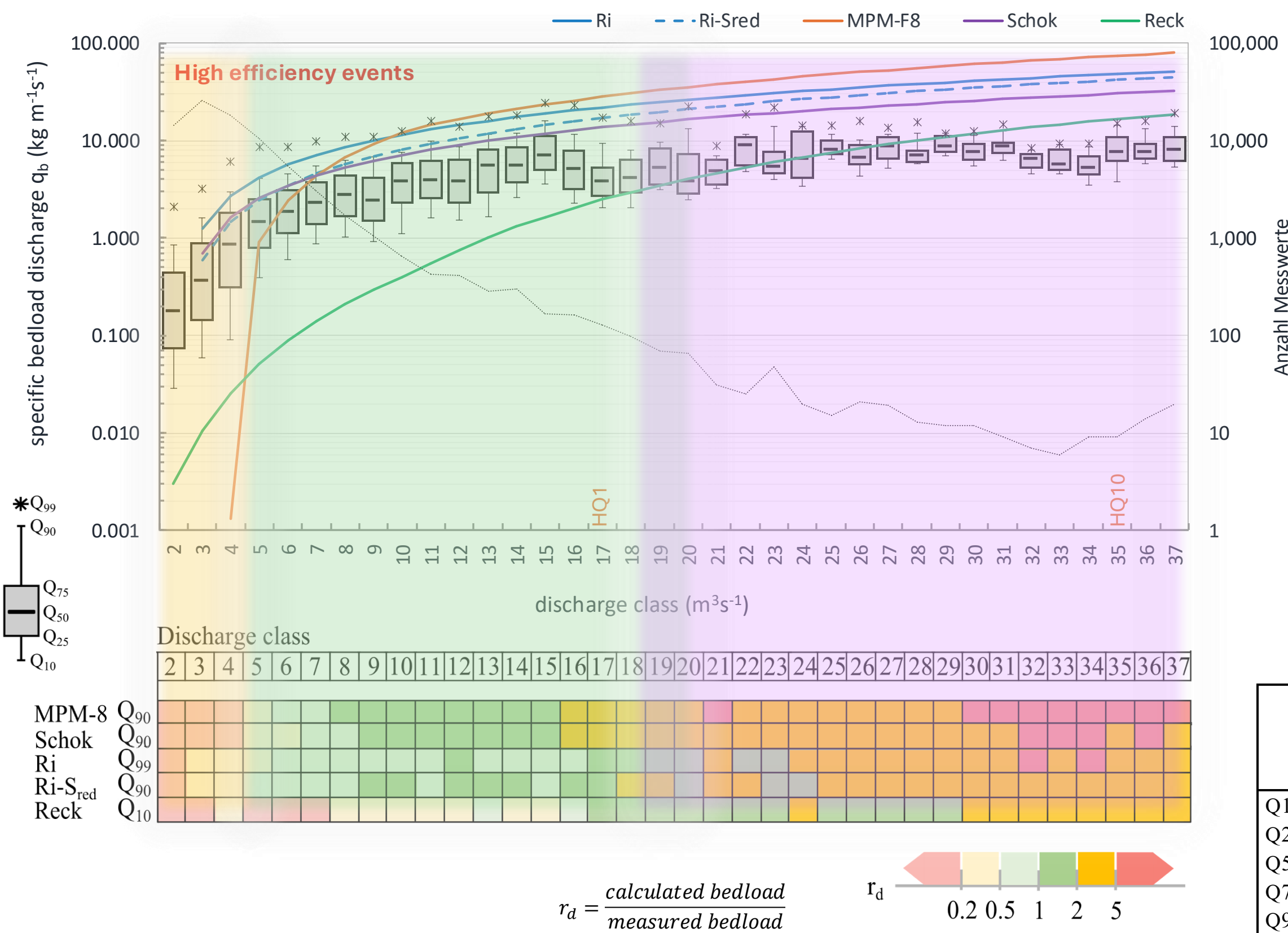
Discrepancy factor

$$r_d = \frac{\text{calculated bedload}}{\text{measured bedload}}$$



Applicability of the formulae could be improved by performing a **classification into event types** after Kreisler et al. (2017), which implies a consideration of **sediment availability**.





Data base: 1min data from 2011-2020
wide range of transport rates for given
flow rates

Underestimation of transport capacity

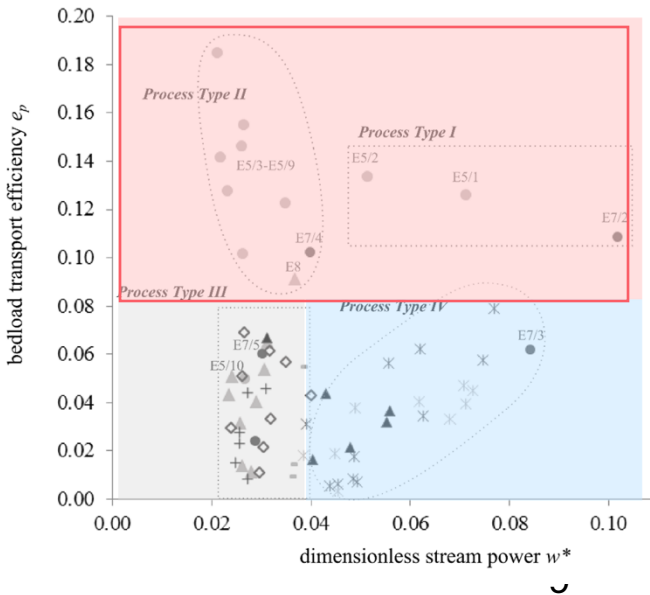
Close agreement

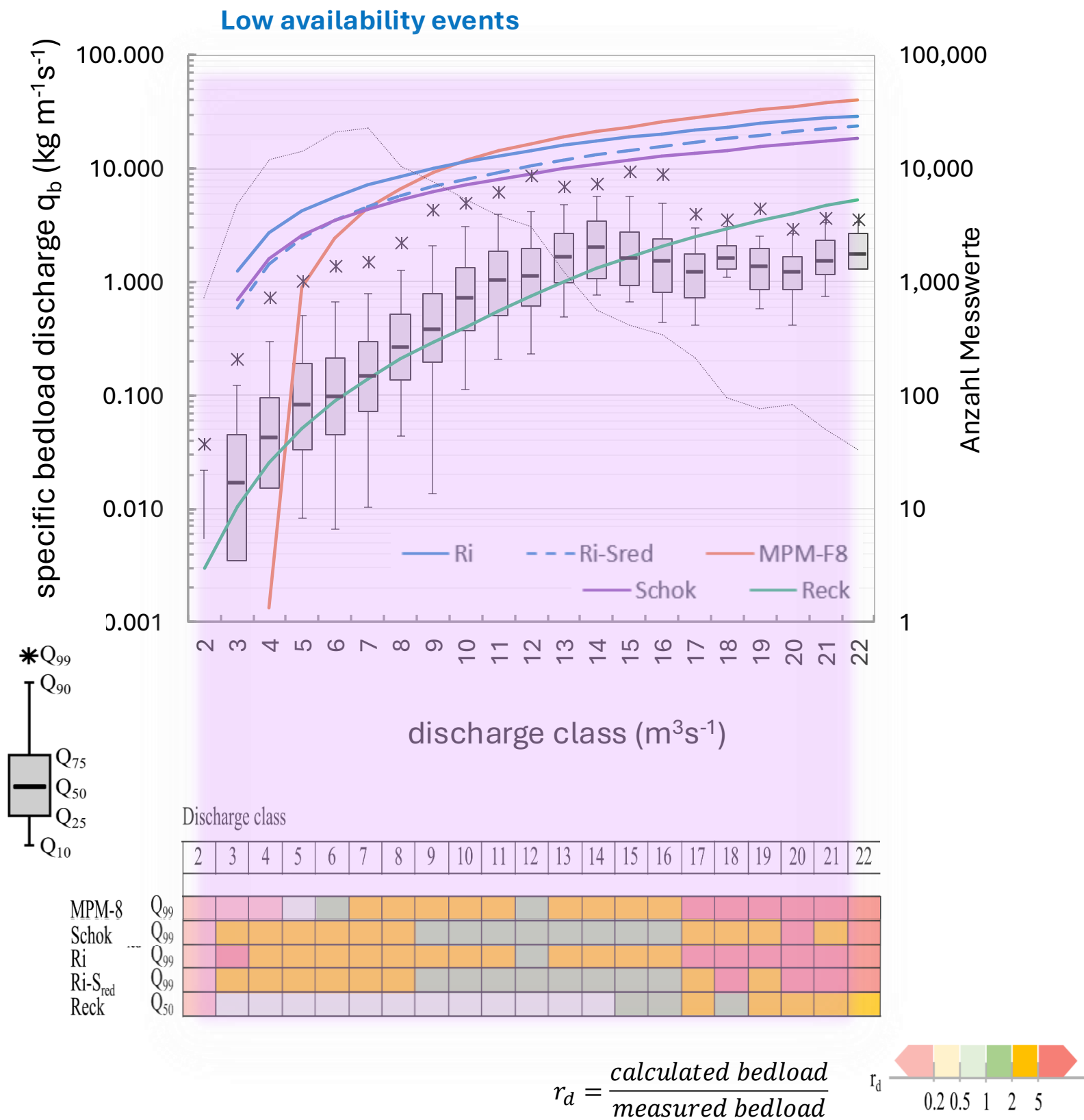
$r_{d \text{ mean DKL 6-20}} :$

- $Ri/Q_{99} = 1.0$
- $Ri S_{red}/Q_{90} = 1.0$
- $MPM-8/Q_{90} = 1.5$
- $Schok/Q_{90} = 0.9$

Overestimation of transport capacity

	RMSLE				
	MPM-8	Schok	Ri	Ri-S _{red}	Reck
Q10	1.6	1.2	1.6	1.3	0.4
Q25	1.3	0.9	1.3	1.0	0.6
Q50	1.0	0.6	1.0	0.7	1.0
Q75	0.8	0.3	0.7	0.4	1.3
Q90	0.7	0.2	0.4	0.3	1.6
Q99	0.8	0.7	0.3	0.6	2.1



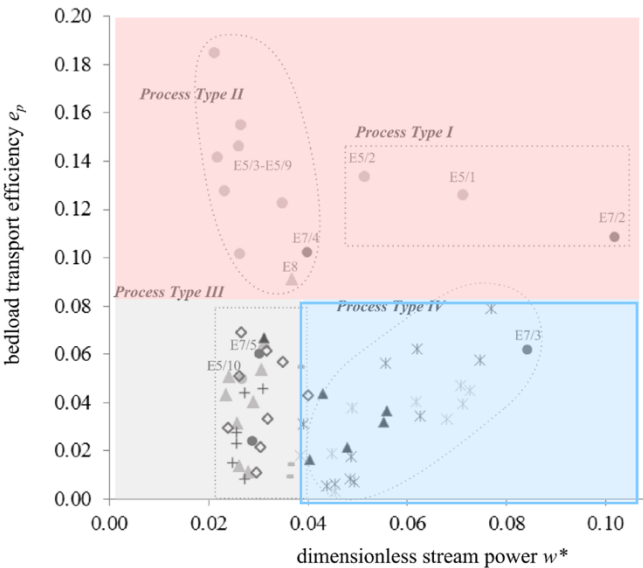


Data base 1min data 2011-2020

Overestimation of measured transport rates

Best Performance - Recking
($r_{d \text{ mean dc 3-17: Reck/Q}_{50}=0.8}$)

	RMSLE				
	MPM-8	Schok	Ri	Ri-S _{red}	Reck
Q10	2.2	1.8	2.2	1.9	0.4
Q25	2.0	1.7	2.1	1.8	0.2
Q50	1.8	1.5	1.9	1.6	0.2
Q75	1.6	1.2	1.6	1.3	0.4
Q90	1.3	1.0	1.4	1.1	0.6
Q99	0.8	0.5	0.9	0.6	1.1



Conclusions

- Combination of direct and indirect measuring devices in the **integrated measuring system** enables comprehensive monitoring of the transport process
- Recording important **continuous long-term data** on natural processes
- Monitored bedload data at the Urslau show a **high variability** – challenges for calculation
- Classification into **event types** considers varying sediment availability
- Applicability of the formulae could be improved by performing a **classification into event types**, good performance of transport capacity based formulas for high efficiency events
- Necessary to select the appropriate formula depending on the given research or management questions
- **Long-term records of integrative measured bedload data are basis for the evaluation and further development of transport formulas** - need for natural measurement data of the bedload transport process!



Thank you for your attention!

Habersack, H., Kreisler, A., Rindler, R., Aigner, J., Seitz, H., Liedermann, M., & Laronne, J. B. (2017).

Integrated automatic and continuous bedload monitoring in gravel bed rivers. *Geomorphology*, 291, 80-93, DOI: 10.1016/j.geomorph.2016.10.020.

Kreisler, A., Moser, M., Aigner, J., Rindler, R., Tritthart, M., & Habersack, H. (2017).

Analysis and classification of bedload transport events with variable process characteristics. *Geomorphology*, 291, 57-68.

Lammer, A., Rindler, R., Tritthart, M., Liedermann, M., Moser, M. Shire-Peterlechner, D. Schwarz, S. & Habersack, H. (2024).

Evaluating the performance of transport equations through long-term records of integrative measured bedload data. *International Journal of Sediment Research*, 40, 158-171.